

(1) Given $\underline{r}(t) = t\mathbf{i} + \cos\left(\frac{\pi}{2}t^2\right)\mathbf{j}$, $0 \leq t \leq 1$

note that $\underline{r}(0) = \mathbf{j}$ (start at $(0,1)$)

$\underline{r}(1) = \mathbf{i}$ (finish at $(1,0)$)

Also, $\underline{F}(x,y) = (1+2xy)\mathbf{i} + (1+x^2)\mathbf{j}$

$F_1 = 1+2xy$, $F_2 = 1+x^2$

$\Rightarrow \frac{\partial F_1}{\partial y} = 2x$, $\frac{\partial F_2}{\partial x} = 2x$

$\Rightarrow \frac{\partial F_1}{\partial y} = \frac{\partial F_2}{\partial x} \Rightarrow \underline{F}$ is conservative

$\Rightarrow \exists \phi(x,y)$ s.t. $F_1 = \frac{\partial \phi}{\partial x}$, $F_2 = \frac{\partial \phi}{\partial y}$

Now $\frac{\partial \phi}{\partial x} = F_1 = 1+2xy \Rightarrow \phi(x,y) = x + x^2y + g(y)$
 $\Rightarrow \frac{\partial \phi}{\partial y} = x^2 + g'(y)$

$= F_2 = 1+x^2$

$\Rightarrow g'(y) = 1 \Rightarrow g(y) = y + C$ (constant C).

$\Rightarrow \phi(x,y) = x + y + x^2y$ is a potential function for $\underline{F}$ (up to constant).

The fundamental theorem of line integrals states that

$$\int_C \underline{F} \cdot d\underline{r} = \phi(\text{finish}) - \phi(\text{start})$$

$$= \phi(1,0) - \phi(0,1)$$

$$= 1 - 1 = 0$$

$$(2) \quad \underline{F}(x, y, z) = 3xy^2 \underline{i} + x \cos z \underline{j} + z^3 \underline{k}$$

$$\text{Net outward flux} = \oint_S \underline{F} \cdot \underline{n} \, dS$$

$$= \iiint_V \underline{\nabla} \cdot \underline{F} \, dV$$

By Gauss' divergence theorem, since all the conditions of the theorem are met by S and $\underline{F}$ & S is the surface of the solid cylinder V .

To describe V , use cylindrical coordinates, but rotated:

$$\left. \begin{array}{l} x \rightarrow y \\ y \rightarrow z \\ z \rightarrow x \end{array} \right\} \text{so} \quad \begin{array}{l} y = r \cos \theta \\ z = r \sin \theta \\ x = r \sin \theta \end{array} \quad \text{\& jacobian still } r.$$

such that

$$V = \{ (x, r, \theta) \mid -1 < x < 2, 0 < \theta < 2\pi, 0 \leq r \leq 1 \}$$

$$\underline{\nabla} \cdot \underline{F} = 3y^2 + 3z^2 = 3r^2$$

$$\Rightarrow \text{flux} = \int_{-1}^2 \int_0^{2\pi} \int_0^1 3r^2 \cdot r \, dr \, d\theta \, dx$$

$$= \left(\int_0^{2\pi} d\theta \right) \left(\int_0^1 3r^3 \, dr \right) \left(\int_{-1}^2 dx \right)$$

$$= 2\pi \times \frac{3}{4} \times (2 - (-1)) = \frac{9}{2} \pi$$

$$(3) \quad \oint_S f(x, y, z) \, ds = \oint_S g(\sqrt{x^2 + y^2 + z^2}) \, ds$$

where S is the surface of the sphere $x^2 + y^2 + z^2 = 9$.

i.e. In $\oint_S$, we are only interested in points on S

$$\Rightarrow \oint_S g(\sqrt{x^2 + y^2 + z^2}) \, ds = \oint_S g(\sqrt{9}) \, ds$$

$$= \oint_S g(3) \, ds$$

$$= \oint_S (-2) \, ds \quad \left(\begin{array}{l} \text{since } g(t) = t - 5 \\ \Rightarrow g(3) = -2 \end{array} \right).$$

$$= -2 \oint_S ds$$

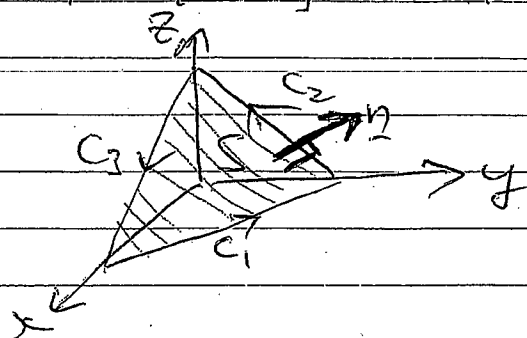
$$= -2 \times (\text{surface area of sphere})$$

$$= -2 \times 4 \times \pi \times 3^2 = -72\pi.$$

(4) Verify $\oint_C \underline{F} \cdot d\underline{r} = \iint_S (\underline{F} \times \underline{F}) \cdot \underline{n} \, dS$.

for $\underline{F} = x\underline{i} + y\underline{j} + xyz\underline{k}$.

& S and $C = C_1 \cup C_2 \cup C_3$ are indicated in the diagram



$C_1: \underline{r}(t) = (1-t)\underline{i} + 2t\underline{j}, \quad 0 \leq t \leq 1$

$\Rightarrow \underline{r}'(t) = -\underline{i} + 2\underline{j} \quad \& \quad \underline{F}(t) = (1-t)\underline{i} + 2t\underline{j}$

$$\begin{aligned} \int_{C_1} \underline{F} \cdot d\underline{r} &= \int_0^1 (\underline{F}(t) \cdot \frac{d\underline{r}}{dt}) dt \\ &= \int_0^1 (-1(1-t) + 4t) dt = -1 + \frac{3}{2} = \frac{1}{2} \end{aligned}$$

$C_2: \underline{r}(t) = 2(1-t)\underline{j} + 2t\underline{k}, \quad 0 \leq t \leq 1$

$\Rightarrow \underline{r}'(t) = -2\underline{j} + 2\underline{k} \quad \& \quad \underline{F}(t) = 2(1-t)\underline{j}$

$$\begin{aligned} \Rightarrow \int_{C_2} \underline{F} \cdot d\underline{r} &= \int_0^1 (\underline{F}(t) \cdot \underline{r}'(t)) dt \\ &= \int_0^1 -4(1-t) dt = -4 + 2 = -2 \end{aligned}$$

$C_3: \underline{r}(t) = t\underline{i} + 2(1-t)\underline{k}$

$\Rightarrow \underline{r}'(t) = \underline{i} - 2\underline{k} \quad \& \quad \underline{F}(t) = t\underline{i}$

$$\begin{aligned} \Rightarrow \int_{C_3} \underline{F} \cdot d\underline{r} &= \int_0^1 (\underline{F}(t) \cdot \underline{r}'(t)) dt \\ &= \int_0^1 t \, dt = \frac{1}{2} \end{aligned}$$

$\oint_C \underline{F} \cdot d\underline{r} = \int_{C_1} + \int_{C_2} + \int_{C_3}$

$$\Rightarrow \oint_C \underline{F} \cdot d\underline{r} = \frac{8}{3} - 2 + \frac{2}{3} = 0.$$

$$\text{Now } \nabla \times \underline{F} = \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ x & y & xyz \end{vmatrix} = xz \underline{i} - yz \underline{j}$$

~~Use $\underline{r}(u,v) = u \underline{i} + v \underline{j}$~~

$$\text{Use } \underline{r}(u,v) = (1-u) \underline{i} + 2u(1-v) \underline{j} + 2uv \underline{k}, \quad 0 \leq u \leq 1, \quad 0 \leq v \leq 1.$$

$$\underline{r}_u = -\underline{i} + 2(1-v) \underline{j} + 2v \underline{k}$$

$$\underline{r}_v = -2u \underline{j} + 2u \underline{k}$$

$$\underline{r}_u \times \underline{r}_v = \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ -1 & 2-2v & 2v \\ 0 & -2u & 2u \end{vmatrix} = 4u \underline{i} + 2u \underline{j} + 2u \underline{k}.$$

(direction of since consistent with orientation of S i.e. has positive $\underline{k}$ component)

$$\& \nabla \times \underline{F}(u,v) = 2u(1-u)v \underline{i} - 4u^2v(1-v) \underline{j}$$

$$\Rightarrow (\nabla \times \underline{F}(u,v)) \cdot (\underline{r}_u \times \underline{r}_v) = 8u^2(1-u)v - 8u^3v(1-v) \\ = 8u^2v - 16u^3v + 8u^3v^2$$

$$\Rightarrow \iint_S (\nabla \times \underline{F}) \cdot \underline{n} \, dS = \int_0^1 \int_0^1 (8u^2v - 16u^3v + 8u^3v^2) \, du \, dv$$

$$= 8 \times \frac{1}{3} \times \frac{1}{2} - 16 \times \frac{1}{4} \times \frac{1}{2} + 8 \times \frac{1}{4} \times \frac{1}{3}$$

$$= \frac{4}{3} - 2 + \frac{2}{3} = 0.$$

$$\text{Hence } \oint_C \underline{F} \cdot d\underline{r} = 0 = \iint_S (\text{curl } \underline{F}) \cdot \underline{n} \, dS$$

in this case.

$$(5) \quad A = \begin{pmatrix} 0 & 1 & 1 & -3 \\ 2 & 6 & 2 & 9 \\ 3 & 1 & 0 & 0 \\ 1 & 3 & 1 & 4 \end{pmatrix} \quad R_1 \leftrightarrow R_4$$

$$\rightarrow \begin{pmatrix} 1 & 3 & 1 & 4 \\ 2 & 6 & 2 & 9 \\ 3 & 1 & 0 & 0 \\ 0 & 1 & 1 & -3 \end{pmatrix} \quad \begin{array}{l} R_2 \rightarrow R_2 - 2R_1 \\ R_3 \rightarrow R_3 - 3R_1 \end{array}$$

Here we use the notation $\textcircled{n}$ in the (i,j) entry means the row operation

$$\rightarrow \begin{pmatrix} 1 & 3 & 1 & 4 \\ \textcircled{2} & 0 & 0 & 1 \\ \textcircled{3} & -8 & -3 & -12 \\ 0 & 1 & 1 & -3 \end{pmatrix} \quad R_2 \leftrightarrow R_4$$

$R_i \rightarrow R_i - nR_j$ was used to make that entry zero (introduced in lectures). This method does not have to be

$$\rightarrow \begin{pmatrix} 1 & 3 & 1 & 4 \\ 0 & 1 & 1 & -3 \\ \textcircled{3} & -8 & -3 & -12 \\ \textcircled{2} & 0 & 0 & 1 \end{pmatrix} \quad R_3 \rightarrow R_3 - (-8)R_2$$

L summarises the row operations (type 2 only) used.

$$\rightarrow \begin{pmatrix} 1 & 3 & 1 & 4 \\ 0 & 1 & 1 & -3 \\ \textcircled{3} & \textcircled{-8} & 5 & -36 \\ \textcircled{2} & 0 & 0 & 1 \end{pmatrix}$$

$$\Rightarrow L = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 3 & -8 & 1 & 0 \\ 2 & 0 & 0 & 1 \end{pmatrix}, \quad U = \begin{pmatrix} 1 & 3 & 1 & 4 \\ 0 & 1 & 1 & -3 \\ 0 & 0 & 5 & -36 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$\text{so that } P_{24}P_{14}A = LU$$

$$\Rightarrow A = P_{14}P_{24}LU = PLU$$

where

$$P = P_{14}P_{24} = \begin{pmatrix} 0 & 0 & 0 & 1 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \textcircled{1} & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \end{pmatrix}$$