

Lec. 24 MATH2100 (= Lec. 6 MATH2011)

Given a scalar field $\varphi(x, y, z)$ and a point $P: (x_0, y_0, z_0)$, the equation

$$\varphi(x, y, z) = \varphi(x_0, y_0, z_0)$$

defines a 2-D surface S passing through P .

On this surface S , $\varphi(x, y, z)$ has the constant value $\varphi(x_0, y_0, z_0)$. We call S a level surface for the field φ . (The level surface that passes through the point P .)

$\nabla\phi$ evaluated at P is a vector $\perp$ to the level surface through P .

direction of $\nabla\phi$ = direction at P of greatest rate of increase of ϕ with changing position.

magnitude $|\nabla\phi|$ = size of greatest rate of increase.

EX1: $\phi(x, y, z) = x^2 + y^2 + z^2$ $P: (1, 2, 3)$

$$\phi(1, 2, 3) = 1 + 4 + 9 = 14$$

$\phi(x, y, z) = 14$ is sphere through P .

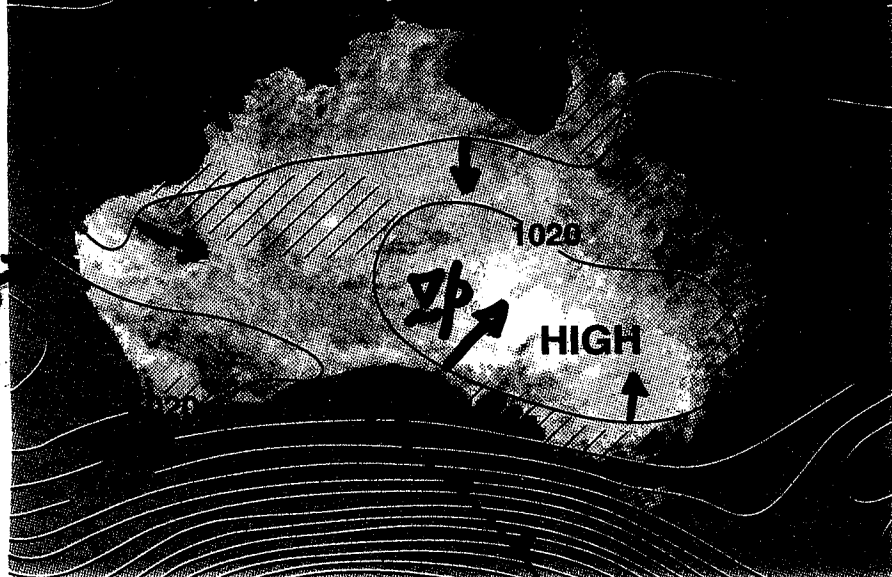
$$x^2 + y^2 + z^2 = 14. \quad \text{Radius } \sqrt{14}$$

$$\nabla\phi = 2x\mathbf{i} + 2y\mathbf{j} + 2z\mathbf{k}$$

EX2:

line of constant
pressure
(isobar)

Isobaric Chart 9pm Friday



7. a

7. a

24.3

$\text{div } \underline{a}$ and $\text{curl } \underline{a}$ give information about the behaviour of $\underline{a}$ as position is changed:-

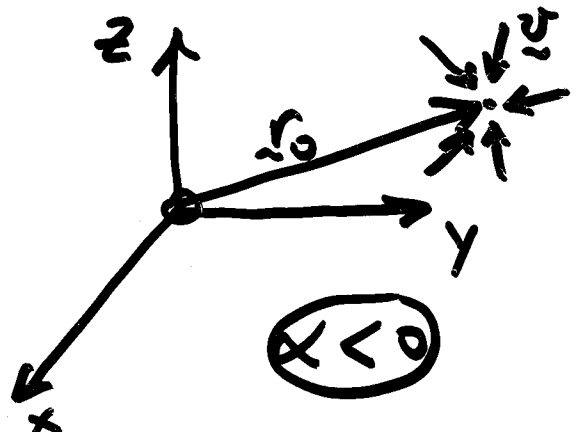
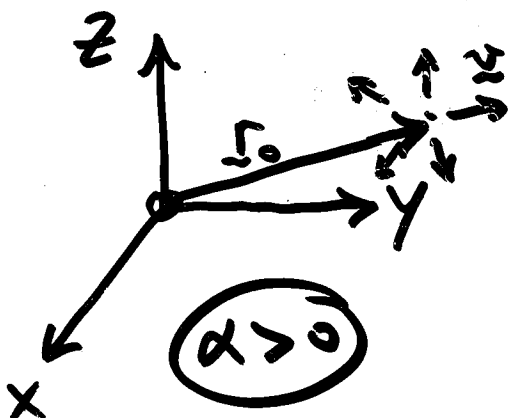
Let $\underline{a} = \underline{v}(x, y, z)$ be velocity field in moving fluid.

$\text{div } \underline{v}$ is measure of tendency of flow to be diverging at any point.

EX: $\underline{v} = \alpha [(x-x_0)\underline{i} + (y-y_0)\underline{j} + (z-z_0)\underline{k}]$

$$\Rightarrow \text{div } \underline{v} = \frac{\partial}{\partial x} [\alpha(x-x_0)] + \frac{\partial}{\partial y} [\alpha(y-y_0)] + \frac{\partial}{\partial z} [\alpha(z-z_0)]$$

$$= \alpha + \alpha + \alpha = 3\alpha$$



$$\underline{r}_0 = x_0 \underline{i} + y_0 \underline{j} + z_0 \underline{k}$$

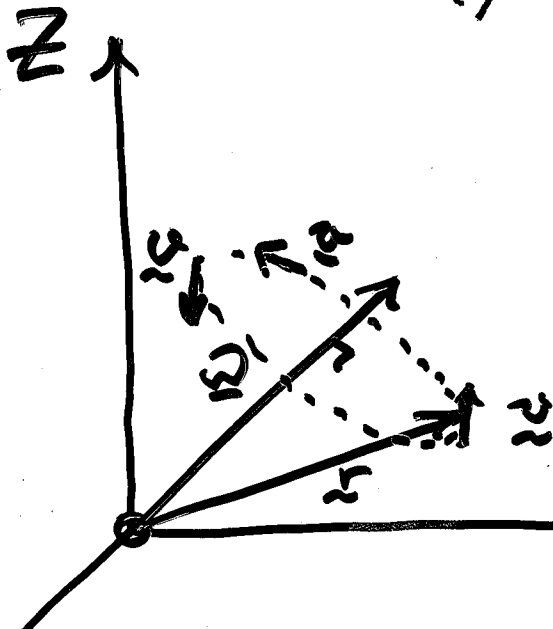
(24.4)

$\text{curl } \underline{v}$ is measure of tendency of flow to be rotating at any point.

EX: $\underline{v} = \underline{\omega} \times \underline{r}$

$$\underline{v} = (\omega_2 z - \omega_3 y) \underline{i} + (\omega_3 x - \omega_1 z) \underline{j} + (\omega_1 y - \omega_2 x) \underline{k}$$

$$\left\{ \begin{array}{l} \underline{\omega} = \omega_1 \underline{i} + \omega_2 \underline{j} + \omega_3 \underline{k} \\ \text{(constant)} \\ \underline{r} = x \underline{i} + y \underline{j} + z \underline{k} \\ \text{(position vector)} \end{array} \right.$$



Fluid rotates about $\underline{\omega}$

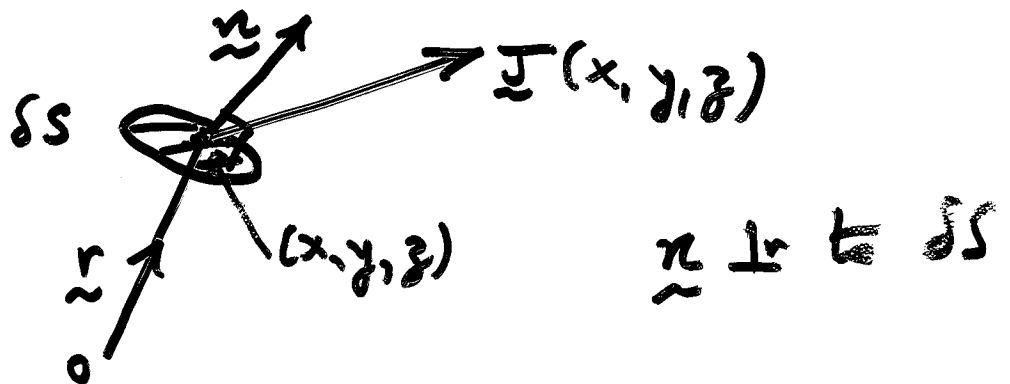
$$\begin{aligned} \text{curl } \underline{v} &= \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \omega_2 z - \omega_3 y & \omega_3 x - \omega_1 z & \omega_1 y - \omega_2 x \end{vmatrix} \\ &= \underline{i}(\omega_1 + \omega_1) - \underline{j}(-\omega_1 - \omega_1) + \underline{k}(\omega_3 + \omega_3) \\ &= 2\underline{\omega} \end{aligned}$$

Flux vector field

When have some substance flowing through space, introduce flux vector field

$$\underline{J}(x, y, z) \quad [\text{or } \underline{J}(x, y, z, t)]$$

Meaning:



$\underline{J} \cdot \underline{n} \delta S$ = amount of substance flowing across δS per unit time.
= flux across δS

EXS: 1) Moving fluid, velocity field $\underline{v}$, density ρ

$\Rightarrow$ mass flux vector $\underline{J} = \rho \underline{v}$

2) Uniform solid, conducting heat.

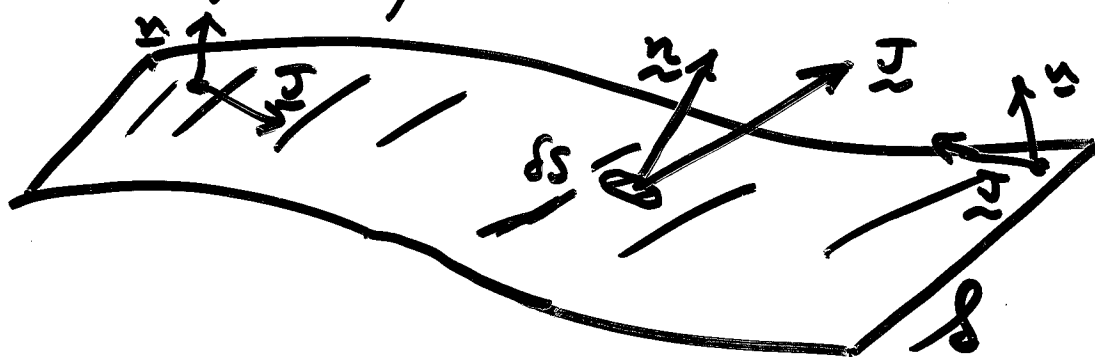
Temperature field T

Thermal conductivity κ

$\Rightarrow$ heat flux vector $\underline{J} = -\kappa \underline{\nabla} T$

(24.6)

When we add the fluxes through all the infinitesimal elements of area making up a surface, we get the flux over the surface (= amount of substance flowing across the surface per unit time).



We write this total flux as

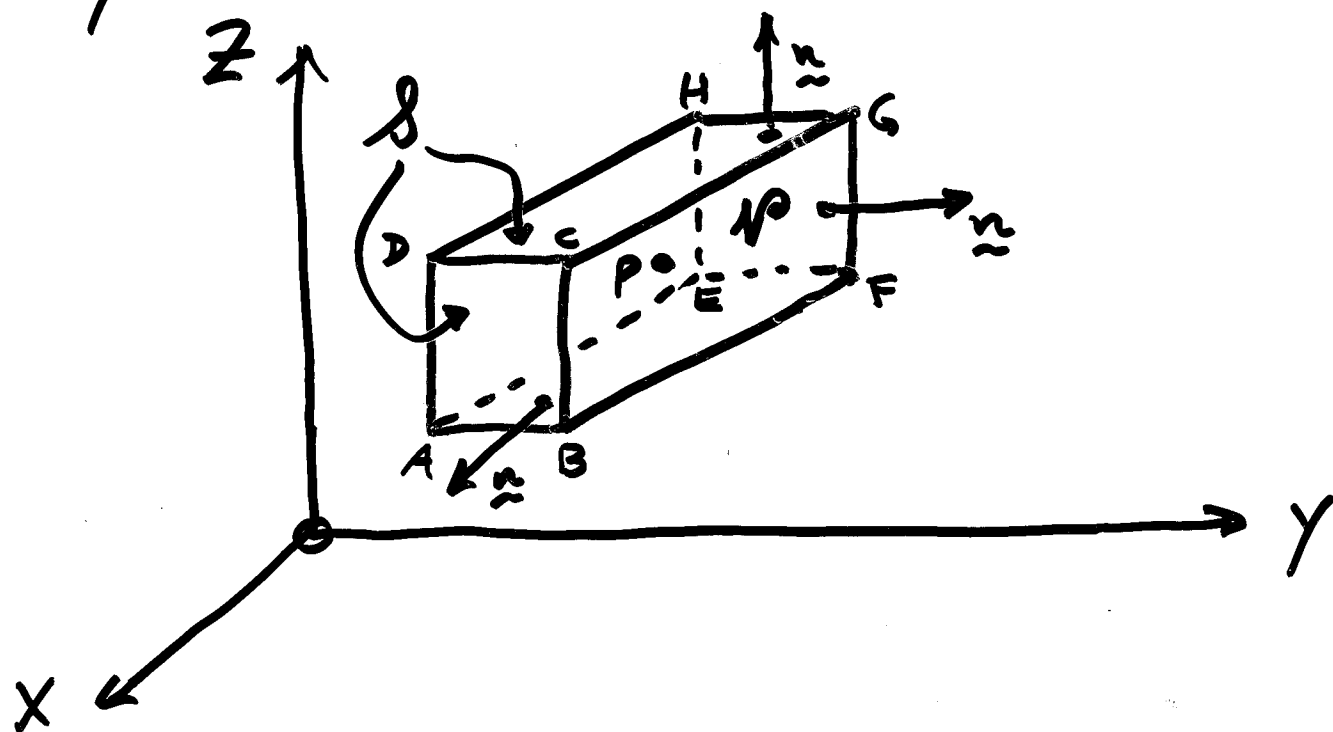
$$\iint_S \underline{J}(x, y, z) \cdot \underline{n}(x, y, z) dS$$

OR simply

$\iint_S \underline{J} \cdot \underline{n} dS$	Flux Integral
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[Write $\oint \underline{J} \cdot \underline{n} dS$ if S is closed.]

Consider what happens when S is surface of small, rectangular box, sides parallel to coordinate axes:-



Suppose $P: (x, y, z)$ is at centre of box, and lengths of sides are $|BF| = 2\Delta x$, $|AB| = 2\Delta y$, $|BC| = 2\Delta z$

⇒ The 3-D region V enclosed by S has volume $\delta V = 8\Delta x \Delta y \Delta z$

Estimate flux out of V over face $ABCD$:

$$\underline{J} \approx \underline{J}(x+\Delta x, y, z) \approx \underline{J}(x, y, z) + \Delta x \frac{\partial \underline{J}(x, y, z)}{\partial x}$$

$$\underline{n} = \underline{i}$$

$$\delta S = 4\Delta y \Delta z$$

$$\begin{aligned} \text{So } \underline{T} \cdot \underline{n} \delta S &\approx \left[T(x, y, z) \underline{i} + \Delta x \frac{\partial T(x, y, z)}{\partial x} \underline{i} \right] 4\Delta y \Delta z \\ &= T(x, y, z) 4\Delta y \Delta z + \frac{\partial T(x, y, z)}{\partial x} 4\Delta x \Delta y \Delta z \end{aligned}$$

Similarly, flux out of V over face EFGH:

$$\underline{T} \approx \underline{T}(x - \Delta x, y, z) \approx \underline{T}(x, y, z) - \Delta x \frac{\partial \underline{T}(x, y, z)}{\partial x}$$

$$\underline{n} = -\underline{i}$$

$$\delta S = 4\Delta y \Delta z$$

$$\Rightarrow \underline{T} \cdot \underline{n} \delta S \approx -T(x, y, z) 4\Delta y \Delta z + \frac{\partial T(x, y, z)}{\partial x} 4\Delta x \Delta y \Delta z$$

So: Flux out over ABCD plus flux out over

$$EFGH \approx \frac{\partial T(x, y, z)}{\partial x} 8\Delta x \Delta y \Delta z = \frac{\partial T(x, y, z)}{\partial x} \delta V$$

Similarly: Flux out over BCGF plus flux out over ADHE $\approx \frac{\partial J_2(x, y, z)}{\partial y} \delta V$

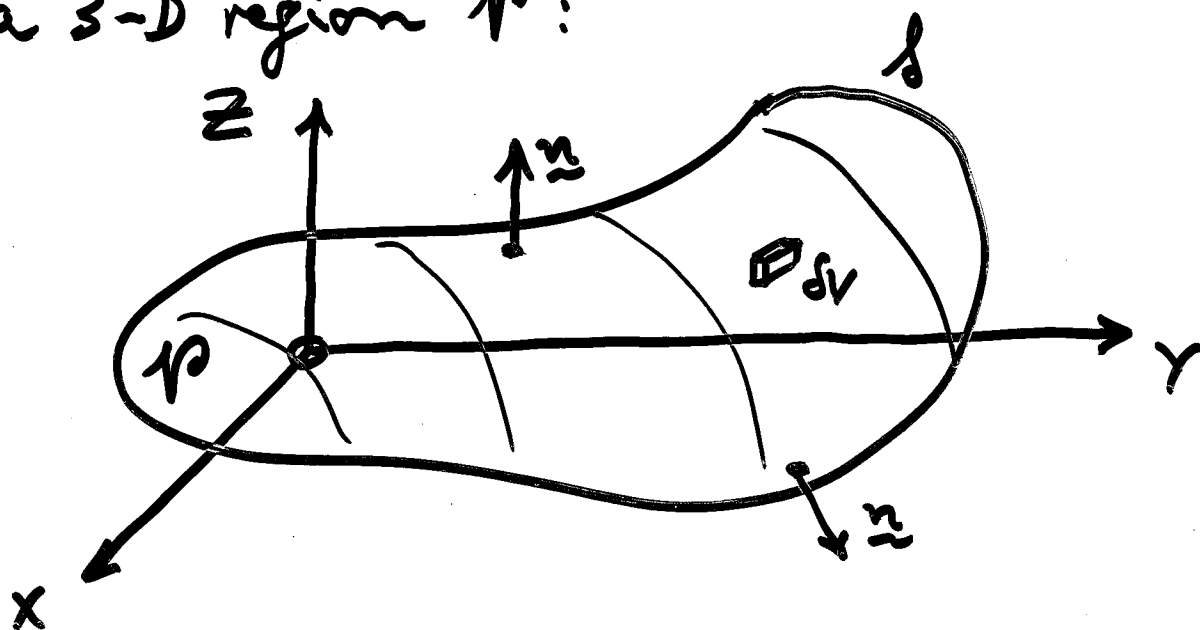
and: Flux out over ABFE plus flux out over DCGH $\approx \frac{\partial J_3(x, y, z)}{\partial z} \delta V$

and so total flux out of V over ∂

$$\approx \left[\frac{\partial J_1(x, y, z)}{\partial x} + \frac{\partial J_2(x, y, z)}{\partial y} + \frac{\partial J_3(x, y, z)}{\partial z} \right] \delta V$$

$$= (\nabla \cdot \underline{J}) \delta V$$

Now consider a general surface ∂ enclosing a 3-D region V :



(24.10)

Imagine dicing V into many tiny rectangular boxes, keeping each in its place.

See sum of outfluxes over all boxes $\approx$ total outflux over S ,
because fluxes over internal faces of boxes cancel in pairs.

$$\text{Now } \sum_{\text{boxes}} \underline{J} \cdot \underline{n} \, \delta S \approx \sum_{\text{boxes}} (\underline{\nabla} \cdot \underline{J}) \, \delta V$$

$$\Downarrow$$
$$\oint_S \underline{J} \cdot \underline{n} \, dS$$

$$\Downarrow$$
$$\iiint_V (\underline{\nabla} \cdot \underline{J}) \, dV$$

Going to limit of infinitesimal boxes we get:

$$\oint_S \underline{J} \cdot \underline{n} \, dS = \iiint_V (\underline{\nabla} \cdot \underline{J}) \, dV$$

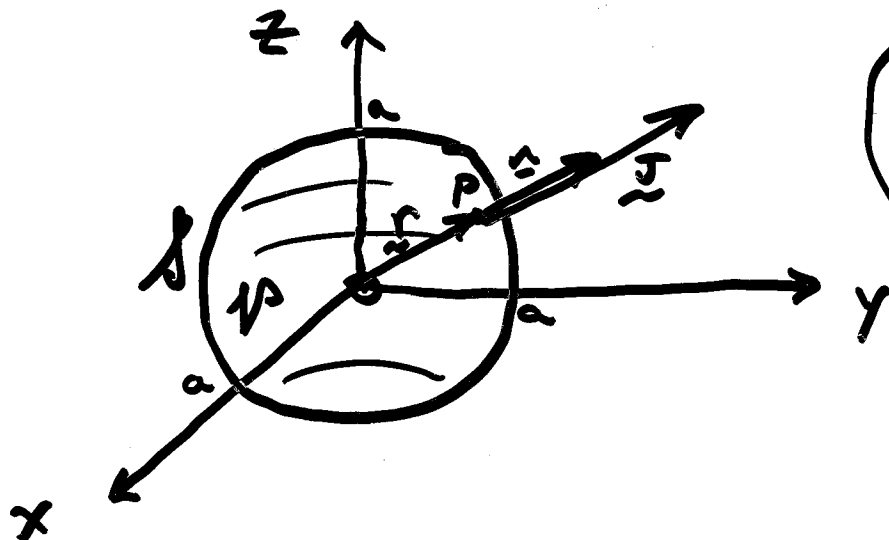
$$(\equiv \iiint_V \text{div } \underline{J} \, dV) \quad (24.1)$$

Gauss' Divergence Theorem

24/11

EX: $\underline{J}(x,y,z) = \alpha(x\underline{i} + y\underline{j} + z\underline{k}) = \alpha\underline{r} \quad (\alpha > 0)$

$(\Rightarrow \nabla \cdot \underline{J} = \alpha + \alpha + \alpha = 3\alpha)$



Take $\mathcal{S}$ = sphere,
radius a
centre O .

At any P on $\mathcal{S}$, see $\underline{r}, \underline{n}, \underline{J}$ all radially outwards.

Then, on $\mathcal{S}$, $\underline{J} \cdot \underline{n} = \alpha \underline{r} \cdot \underline{\hat{r}} = \alpha |\underline{r}| = \alpha a$

Then $\iint_{\mathcal{S}} \underline{J} \cdot \underline{n} \, ds = \alpha a \iint_{\mathcal{S}} ds = \alpha a (4\pi a^2) = 4\pi \alpha a^3$

and $\iiint_V (\nabla \cdot \underline{J}) \, dv = 3\alpha \iiint_V dv = 3\alpha \left(\frac{4}{3}\pi a^3\right) = 4\pi \alpha a^3$

It works!

Summary:

- 1) Understand definitions and meanings of $\text{grad } \varphi$, $\text{div } \underline{a}$ and $\text{curl } \underline{a}$.
- 2) Understand notion of a flux vector field.
- 3) Understand notion of a flux integral
- 4) Know Gauss' Divergence Theorem (not proof).

~~K p. 481, § 9.7, 9.8~~

K § 10.6, 10.7, 10.8